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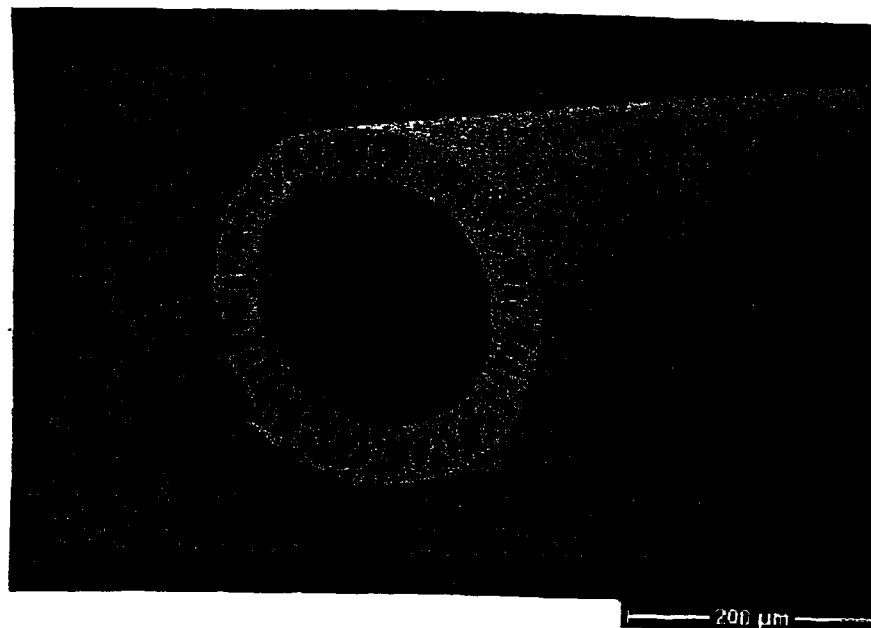
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(54) Title: PERM SELECTIVE ASYMMETRIC HOLLOW FIBRE MEMBRANE FOR THE SEPARATION OF TOXIC MEDIATORS FROM BLOOD



(57) Abstract: The present invention relates to a permselective asymmetric hollow fibre membrane for the separation of toxic mediators from blood, comprised of at least one hydrophobic polymer and at least one hydrophilic polymer. Further, the present invention relates to a process for the preparation of such a membrane, and the use of said membrane in hemodialysis, hemodiafiltration and hemofiltration for treatment of toxic mediator related diseases.

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Perm selective Asymmetric Hollow fibre Membrane for the Separation of Toxic Mediators from Blood.

Technical field of the invention

The present invention relates to a permselective asymmetric hollow fibre membrane for the separation of
5 toxic mediators from blood, comprised of at least one hydrophobic polymer and at least one hydrophilic polymer. Further, the present invention relates to a process for the preparation of such a membrane, and the use of said membrane in hemodialysis, hemodiafiltration and
10 hemofiltration for treatment of toxic mediator related diseases.

Background of the invention

A significant number of patients in intensive care
15 units die from a secondary complication known commonly as "sepsis" or "septic shock". Medical illness, trauma, complication of surgery, and any human disease state, if sufficiently injurious to the patient, may develop into systemic inflammatory response syndrome ("SIRS"), multi-
20 organ system dysfunction syndrome ("MODS"), and multi-organ system failure ("MOSF").

The mechanism of SIRS is the excessive release of host derived inflammatory mediators, herein referred to as toxic mediators ("TM"). TM include various cytokines
25 (tumor necrosis factor, TNF; the interleukins; interferon), various prostaglandins (PG I.sub.2, E.sub.2, Leukotrienes), various clotting factors (platelet activating factor, PAF), various peptidases, reactive oxygen metabolites, and various poorly understood peptides which
30 cause organ dysfunction (myocardial depressant factor, MDF). If the inflammatory response is excessive, then injury or destruction to vital organ tissue may result in

multiorgan dysfunction syndrome ("MODS"). Sepsis is the single most common cause of SIRS leading to MOSF.

Hemofiltration ("HF") was developed as a technique to control overhydration and acute renal failure in unstable patients and may use a hemofilter consisting of a cellulose derivatives or synthetic membrane (e.g., polysulfone, polyamide, etc.) fabricated as either a parallel plate or hollow fibre filtering surface. Current HF membranes, when used to treat acute renal failure associated with MOSF have been associated with incidental improvements in organ function other than the kidneys. However, these membranes remain deficient in the treatment of MOSF because their specific design characteristics prevent them from removing TM in the upper molecular weight range of recognized TM.

The pores of most conventional hemofiltration membranes allow passage of molecules up to 30,000 Daltons in water with very few membranes allowing passage of molecules up to 50,000 Daltons. The membranes used to treat renal failure were generally designed to achieve the following specific goals: (i) to permit high conductance of the aqueous phase of blood plasma water needed to permit the formation of ultrafiltrate at a fairly low transmembrane pressure (typically 20-40 mm Hg), which requires a relatively large pore size that incidentally passes molecules of up to 30,000 to 50,000 Daltons; and (ii) to avoid passage of albumin (e.g., 68,000 Daltons). Loss of albumin, and subsequently, oncotic pressure, could cause or aggravate tissue oedema and organ dysfunction (e.g., pulmonary oedema), so hemofilters are often designed to avoid this by having molecular weight exclusion limits well below the molecular weight of albumin (e.g., 68,000 Daltons).

During filtration of protein containing solutions, after only 20 min the accumulation of protein as a gel or polarization layer occurs on the membrane surface. This gel layer dramatically reduces effective pore size,

reducing the filterable molecular weights by roughly 10-40%. Therefore, pore sizes selected are somewhat larger than needed, anticipating a reduction in effective size.

US-A-5 571 418 discloses a novel method of
5 continuous arteriovenous hemofiltration (CAVH) using a polysulfone or similar material, hollow fibre hemofilter with a molecular weight exclusion limit of up to 100,000 to 150,000 Daltons as therapeutic regimen for sepsis, multiple organ failure (MOF), systemic inflammatory re-
10 sponse syndrome (SIRS) or other mediator-related diseases.

The device and process described in US-A-5,571,418 generally contemplates the use of large pore hemofiltration membranes with pore sizes to provide molecular
15 weight exclusion limits of 100,000 to 150,000 Daltons in water. With these higher molecular weight cut-offs, these membranes are designed to remove a wider range of different IM's.

EP-A-0 305 787 discloses permselective assymmetric
20 membranes suitable for hemodialysis and a process for the manufacturing thereof. Said membrane has a special three-layer structure having high diffusive permeability, comprising a first inner layer in the form of a dense rather thin skin, having a thickness below 1 μm and a
25 maximum pore size of about 8 nm, responsible for the sieving properties, a second layer in the form of a sponge structure, having a thickness of about 1 to 15 μm and serving as a support for said first layer and a third layer in the form of a finger structure, giving the
30 membrane a mechanical stability and having a thickness of about 20 to 60 μm . The membrane is manufactured by presolving the hydrophobic first polymer in a solvent, presolving the hydrophilic second polymer in a solvent of preferably the same kind, mixing the two solutions,
35 extruding the mixture through the outer ring slit of a nozzle with two concentric openings, a precipitating liquid including a part of the hydrophilic second polymer

flowing through the inner openings, to obtain a coagulated membrane, which is subsequently washed and preferably dried.

5 Summary of the invention

 The object of the present invention is to provide an improved permselective asymmetric hollow fibre membrane for the separation of toxic mediators from blood, comprised of at least one hydrophobic polymer and at
10 least one hydrophilic polymer.

 This object is achieved by a membrane, which allows passage of molecules having a molecular weight of 45 000 Daltons in presence of whole blood and having a molecular weight exclusion limit in water of about 200,000 Daltons.

15 A further object of the invention is to provide a process for the preparation of the membrane of the present invention.

 This object is achieved by a process comprising the steps of

- 20 a) dissolving the at least one hydrophobic polymer and the at least one hydrophilic polymer in a solvent to form a polymer solution,
- b) extruding the formed polymer solution through an outer ring slit of a nozzle with two concentric openings,
- 25 c) extruding a centre fluid through the inner opening of the nozzle, and
- d) subsequently washing and preferably drying the membrane, wherein the polymer solution comprises 10-20 weight% hydrophobic polymer and 2-11 weight% hydrophilic
30 polymer.

 Yet another object of the invention is to provide a use of the membrane for treatment of toxic mediator related diseases, especially sepsis, in hemodialysis mode, hemodiafiltration mode and hemofiltration mode.

35 The present invention comprises HD, HDF and HF methods using a novel membrane fabricated with a pore size capable of allowing passage of molecules of about

45,000 Daltons in presence of whole blood and having an exclusion limit in water of about 200,000 Daltons. The membrane of the present invention is useful in treating human patients with SIRS-MOSF and provides for removal by
5 filtration and/or diffusion of the entire known range of TM.

By the membrane of the invention a high selectivity is achieved, i. e. a high removal of toxic mediators having a molecular weight of up to 45,000 Dalton is
10 achieved at the same time as a low amount of albumin, having a molecular weight of 68,000 Dalton is lost. Moreover, the risk for proteins which penetrate into the membrane structure to be absorbed in the pore structure of the membrane and thus change the permeability of the
15 membrane, is highly reduced.

Other objects, features, advantages and preferred embodiments of the present invention will become apparent from the following detailed description when taken in conjunction with the drawings and the appended claims.
20

Brief description of the drawings

Preferred embodiments of the present invention will now be described in more detail, reference being made to the enclosed drawings, in which:

25 Fig. 1a and 1b show scanning electron microscopic pictures of cross sections of the membrane structure according to a preferred embodiment of the invention,

Fig 2 shows a scanning electron microscopic picture of the inner surface of the membrane,

30 Fig 3a and 3b shows the sieving coefficients for two different membranes, a prior art standard "high flux membrane" and the membrane according to the invention,

Fig 4 shows the protein loss into the filtrate for a standard high flux membrane and for the membrane of the
35 invention,

Fig 5 shows IL-6 values in plasma and filtrate 30 min after initiation of filtration by the membrane of the invention, and

Fig 6 shows the removal of circulating mediators in
5 Renal Intensive Care (RIC)/sepsis for a standard high flux membrane and the membrane of the invention.

Detailed description of preferred embodiments

The present invention provides a permselective asym-
10 metric hollow fibre membrane for use in a method of treating a pathophysiological state by filtering and/or dialysing blood, comprising the steps of: withdrawing blood from a mammal; filtering and/or dialysing the blood; and returning said blood to the mammal. The
15 methods of the present invention may use either continuous arteriovenous or continuous venovenous hemofiltration, hemodiafiltration or hemodialysis.

As used herein, the term "hemodialysis", HD, refers to a process to correct the chemical composition of blood
20 by removing accumulated metabolic products and adding buffer in a process of diffusion through a natural or synthetic semi-permeable membrane.

As used herein, the term "hemodiafiltration", HDF, refers to a process to remove accumulated metabolic
25 products from blood by a combination of diffusive and convective transport through a semi-permeable membrane of high-flux type; fluid is removed by ultrafiltration and the volume of filtered fluid exceeding the desired weight loss is replaced by sterile, pyrogen-free infusion
30 solution.

As used herein, the term "hemofiltration", HF, refers to a process of filtering blood by a membrane with separation of plasma water and solutes with the ultrafiltrate, and retains all proteins larger than
35 effective pore size and blood cells. In hemofiltration the accumulated metabolic products are removed from the blood by the process of convective transport as a

consequence of ultrafiltration through a semi-permeable membrane of high-flux type; the volume of filtered fluid exceeding the desired weight loss is replaced by sterile pyrogen-free infusion solution.

5 As used herein, the term "ultrafiltrate" refers to the filtered plasma water and solute and molecules (including target peptides and proteins) smaller than effective pore size.

10 The term "hollow fibre membrane" used throughout the application text is intended to cover everything from one single hollow fibre up to several single hollow fibres and one or more bundles of such hollow fibres, each fibre having a filtrate side and a blood side.

15 The term "flat sheet membrane" used throughout the application text means a micropore containing flat membrane having a filtrate side and a blood side.

20 As used herein, the term "Toxic Mediators", TM, refers to a heterogeneous group of chemicals synthesized and released by human tissue. TM include the inflammatory mediators of SIRS (cytokines, prostaglandins, oxygen metabolites), various clotting factors, various peptidases and various toxic peptides. The molecular weight range of known TM is 1,000-60,000.

25 As used herein, the term "hemofilter", refers to the filter used in hemofiltration. It is configured as either a series of parallel plates or as a bundle of hollow fibres. The blood path is from a blood inlet port, through the fibres or between the plates, then to a blood outlet port. Filtration of blood occurs at the membrane
30 with ultrafiltrate forming on the side of the membrane opposite the blood. This ultrafiltrate accumulates inside the body of the filter contained and embodied by the filter jacket. This jacket has an ultrafiltrate drainage port.

35 As used herein, the term "hemodialyser", refers to the semi-permeable membrane used in hemodialysis. It is configured as either a series of parallel plates or as a

bundle of hollow fibres. The blood path is from a blood inlet port, through the fibres or between the plates, then to a blood outlet port. A dialysate path is from a dialysate inlet port, outside the fibres or between the plates, then to a spent dialysate drain port. The dialysing of blood occurs at the membrane by diffusion through the membrane from the blood side to the dialysate side, and adding of buffer from the dialysate side to the blood side. The dialysate comprising necessary buffer and electrolytes.

As used herein, the term "extracorporeal circuit" refers to the system of plastic tubes attached to the hemofilter which is used clinically. The arterial line is the plastic tube which carries blood from artery or vein to the blood inlet port of the hemofilter. The venous line carries blood from the blood outlet port returning to a vein. The ultrafiltrate line carries ultrafiltrate from the ultrafiltrate drainage port on the filter jacket to a reservoir from which ultrafiltrate is discarded.

As used herein, the term "effective sieving coefficient (S)" refers to the physical property of a membrane to exclude or pass molecules of a specific molecular weight:

$$S = (\text{concentration in filtrate}) / (\text{concentration in feed})$$

For the purposes of the present invention, the appropriate membrane allows for passage of molecules in the range of toxic mediators of up to 45,000 Daltons in the presence of whole blood/blood proteins, which means the molecular weight of a substance having a sieving coefficient (S) of 0.1 -1.0 in presence of whole blood.

As used herein the term "cut off" refers to "nominal cut off" which means the molecular weight of a substance having a sieving coefficient (S) of 0.1 in water.

The membrane, in a preferred embodiment of the present invention has a unique structure, including a

specific 3-layer structure with an innermost layer, i. e. a blood contacting layer, having a glomerular structure of the skin with pores having a size in the nanoscale range. In Fig 1a and 1b cross sections of the membrane structure according to the invention are shown, and in
5 Fig 2 a scanning electron microscopic picture of the inner surface of the membrane. Pore channels between glomerular polymer clusters consisting of a mixture of hydrophilic polymers and hydrophobic polymers are shown.

10 At least one hydrophilic polymer and at least one hydrophobic polymer are present in the membrane as domains on the surface. Preferably the hydrophobic polymer is present in an amount of 10-20 weight%, based on the weight of the membrane. The hydrophilic polymer is
15 preferably present in an amount of 2-11 weight%, based on the weight of the membrane.

The hydrophobic polymer according to the invention may be chosen from the group consisting of polyarylether-sulfone (PAES), polypropylene (PP), polysulfone (PSU),
20 polymethylmethacrylate (PMMA), polycarbonate (PC), polyacrylonitrile (PAN), polyamide (PA), or polytetrafluoroethylene (PTFE).

The hydrophilic polymer of the invention may be chosen from the group consisting of polyvinylpyrrolidone
25 (PVP), polyethyleneglycol (PEG), polyvinylalcohol (PVA), and copolymer of polypropyleneoxide and polyethyleneoxide (PPO-PEO).

The membrane of the invention has in a preferred embodiment at least a 3-layer asymmetric structure. In
30 the innermost layer of the hollow fibre a separation layer is present, having a thickness of $< 0.5 \mu\text{m}$ and containing pore channels, having a pore size of 15-60 nm, preferably 20-40 nm. The next layer in the hollow fibre membrane is the second layer, having the form of a sponge
35 structure and in a preferred embodiment a thickness of about 1-15 μm and serving as a support for said first layer. Then, there is the third layer, having the form of

a finger structure. It provides like a framework a mechanical stability on the one hand; on the other hand it has through the high void volume a very low resistance of transport of molecules through the membrane. During
5 the process the voids are filled with water and the water gives a lower resistance against diffusion and convection than a matrix with a sponge-filled structure having a lower void volume. Accordingly, the third layer gives the membrane a mechanical stability and has, in a preferred
10 embodiment of the present invention, a thickness of 20 to 60 μm .

In Fig 3 the sieving coefficients for two different membranes, a prior art standard "high flux membrane" and the high cut off membrane according to the invention are
15 shown. In Fig 4 the protein loss is illustrated. As may be seen from the figures the sieving coefficient of the membrane according to the present invention is superior to the high flux membrane and at the same time the loss of albumin is significantly lower in the membrane of the
20 invention. According to a preferred embodiment of the invention the sieving coefficient for albumin in presence of whole blood is below 0,05.

Fig 5 and Fig 6 shows the removal of circulating mediators in Renal Intensive Care (RIC)/sepsis. According
25 to the invention the sieving coefficient for IL-6 in presence of whole blood is 0.9-1.0. In a preferred embodiment the membrane having the above described three-layer structure also includes a fourth layer, which is the outer surface of the hollow fibre membrane. In this
30 preferred embodiment the outer surface has openings of pores in the range of 0.5-3 μm and the number of said pores are in the range of 10,000 to 150,000 pores/ mm^2 , preferably 20,000 to 100,000 pores/ mm^2 . This fourth layer preferably has a thickness of 1 to 10 μm .

35 An advantage of these embodiments is the provision of a hollow fibre membrane, which is non-sticky and is easy to handle. This results in less cracks and holes in

the fibres during the manufacturing process, which in turn leads to less scrap in the manufacturing process. Another advantage is that the hollow fibre has less tendency to adhere to the hollow fibres adjacent in the bundle due to the high number of pores on the surface. Thus, the dialysate surrounding the hollow fibres during use has enhanced access to the hollow fibres since they are less inclined to adhere to each other.

This specific surface on the outside of the hollow fibre is achieved by modifying the spinning polymer solution composition only in the outer section of the hollow fibre membrane wall by penetration of water from a very specific steam/air atmosphere into the first 1-15 μm of polymer solution layer just before the precipitation from the inside arrives at this layer.

The manufacturing of the membrane according to the present invention follows a phase inversion process, wherein a polymer or a mixture of polymers is dissolved in a solvent to form a polymer solution. The solution is degased and filtered and is thereafter kept at an elevated temperature.

Subsequently, the polymer solution is extruded through a spinning nozzle (for hollow fibres) or a slit nozzle (for flat film) into a fluid bath containing a nonsolvent for the polymer. The nonsolvent replaces the solvent and thus the polymer is precipitated to an inverted solid phase.

In the present invention the polymer solution preferably is extruded through an outer ring slit of a nozzle having two concentric openings. Simultaneously a centre fluid is extruded through an inner opening of the nozzle. At the outlet of the spinning nozzle the centre fluid comes in contact with the polymer solution and at this time the precipitation is initialised. The precipitation process is an exchange of the solvent from the polymer solution with the nonsolvent of the centre fluid. Through this exchange the polymer solution inverses its

phase from the fluid into a solid phase. In the solid phase there is built, by the kinetic of the solvent/nonsolvent exchange, the pore structure, i. e. asymmetry and the pore size distribution. The process works at a certain temperature which influences the viscosity of the polymer solution. According to the invention the temperature at the spinning nozzle and of the polymer solution and centre fluid is 30-80°C. The viscosity determines the kinetic of the pore forming process through the exchange of solvent with nonsolvent. Subsequently, the membrane is preferably washed and dried.

By the selection of precipitation conditions, e. g. temperature and speed, the hydrophobic and hydrophilic polymers are "frozen" in such a way that a certain amount of hydrophilic end groups are located at the surface of the pores and create hydrophilic domains. The hydrophobic polymer builds other domains. A certain amount of hydrophilic domains at the pore surface area are needed to avoid adsorption of proteins. The size of the hydrophilic domains should preferably be within the range of 20-50 nm. In order to repel albumin from the membrane surface the hydrophilic domains also need to be within a certain distance from each other. By the repulse of albumin from the membrane surface direct contact of albumin with the hydrophobic polymer is avoided and consequently the absorption of albumin.

The polymer solution preferably comprises 10-20 weight% of hydrophobic polymer and 2-11 weight% of hydrophilic polymer. The centre fluid comprises 45-60 weight% of precipitation medium, chosen from the group of water, glycerol and other alcohols, and 40-55 weight% of solvent. In other words, the centre fluid does not comprise any hydrophilic polymer.

In a preferred embodiment of the invention the polymer solution coming out through the outer slit openings is, on the outside of the precipitating fibre, exposed to

a humid steam/air mixture. Preferably, the humid steam/air mixture has a temperature of at least 15°C, more preferably at least 30°C, and not more than 75°C, more preferably not more than 60°C.

5 Preferably, the relative humidity in the humid steam/air mixture is between 60 and 100%

 Furthermore, the humid steam in the outer atmosphere surrounding the polymer solution emerging through the outer slit openings, preferably includes a solvent. The
10 solvent content in the humid steam/air mixture is preferably between 0,5 and 5 weight% related to the water content. The effect of the solvent in the temperature controlled steam atmosphere is to control the speed of precipitation of the fibres. If less solvent is employed
15 the outer surface will obtain a more dense surface, and if more solvent is used the outer surface will be more open structure. By controlling the amount of solvent within the temperature controlled steam atmosphere surrounding the precipitating membrane, the amount and
20 size of the pores on the outer surface of the membrane are controlled, i. e. the size of the openings of the pores are in the range of 0.5-3 μm and the number of said pores are in the range of 10,000 to 150,000 pores/ mm^2 , preferably 20,000 to 100,000 pores/ mm^2 . The fourth layer
25 of the membrane is preferably prepared by this method.

 Before the extrusion suitable additives may be mixed into the mixture of the polymer solution. The additives are used to form a proper pore structure and optimise therewith the membrane permeability, the hydraulic and
30 diffusive permeability and the sieving properties. The additives may be said to work as pore controller. In a preferred embodiment of the invention the polymer solution contains 0.5-7.5 weight% of a suitable additive, preferably chosen from the group comprising water, glycerol and other alcohols.
35

 According to the invention the solvent may be chosen from the group comprising, n-methylpyrrolidon (NMP), di-

methylacetamid (DMAC), dimethylsulphoxide (DMSO) dimethylformamide (DMF), butyrolactone and mixtures of said solvents.

According to a preferred embodiment of the invention, the conditions on the outside of the membrane and the combination with the polymer composition, centre fluid and temperature of the spinning nozzle, creates the optimal structure in a membrane according to the invention, i. e. four integral layers. Depending on the ratio of the components the four layers get different thickness.

It will be readily apparent to one skilled in the art that various substitutions and modifications may be made to the invention disclosed herein without departing from the scope and spirit of the invention.

The present invention will now be illustrated by way of non-limiting examples of preferred embodiments in order to further facilitate the understanding of the invention.

Examples

Example 1

A polymer solution is prepared by mixing 14 weight% of polyarylethersulfone, 0.5 weight% of polyamide, 8 weight% of PVP K30, 2 weight% of water and 75.5 weight% of NMP. A mixture of 52 weight% water and 48 weight% NMP serves as a centre and precipitation solution. The viscosity of the polymer solution, measured at a temperature of 22°C is 4,5 Pas.

The centre and polymer solution are heated to 57°C and pumped towards a 2-component hollow fibre spinneret. The polymer solution emerges from the spinneret through an annular slit with an outer diameter of 0.5 mm and an inner diameter of 0.35 mm. The centre solution emerges from the spinneret in the centre of the annular polymer solution tube in order to start the precipitation of the

polymer solution from the inside and to determine the inner diameter of the hollow fibre.

At the same time the 2 components (polymer & centre solution) enters a space separated from the room atmosphere. This space is called spinning shaft. A mixture of steam (100°C) and air (22°C) is injected into the spinning shaft. The temperature in the spinning shaft is adjusted by the ratio of steam and air at 52°C. The relative humidity was adjusted to 98 % and the solvent content was controlled to 4.5 % by weight NMP related to water content. The length of the spinning shaft is 890 mm. By the aid of gravity and a motor-driven roller, the hollow fibre is drawn from top to bottom, from spinneret through the spinning shaft into a water bath in vertical direction. The spinning velocity is 15.0 m/min. The hollow fibre is subsequently led through a cascade of water bathes and temperatures increasing from 20 to 90°C. The wet hollow fibre membrane leaving the water rinsing bath is dried in a consecutive online drying step. After a texturising step, the hollow fibre is collected on a spinning wheel in the shape of a bundle. After introducing the bundle into a dialyser housing, it is potted with polyurethane, ends are cut, on both sides of the dialyser a header is fixed to the housing, the dialyser is rinsed with hot water and dried with air. During this last drying step, an amount of 19 g of residual water per m² effective membrane area is left on the dialyser. The filter device contains 1,1 m² effective membrane area. After labelling and packaging, the dialyser is steam-sterilized within the package in an autoclave at 121°C for 25 min.

Example 2 (Comparative)

Compared to example no. 1, only the following was changed in the composition of the polymer solution : 16 % of polyarylethersulfone, 0.5 % of Polyamide, 8 % of PVP K30, 0% of water and 75.5 % of NMP.

The composition of the centre solution was changed to: 48 % water and 52 % NMP .

The polymer solution temperature was 46°C, and the spinning shaft temperature was 42°C.

5

Example 3 (Comparative)

Compared to example no. 1, only the following was changed in the composition of the polymer solution: 14% of polyarylethersulfone, 0.5% of polyamide, 7% of PVP K30, 3% of water, and 75.5% of NMP.

10

The composition of the centre solution was changed to: 60% water and 40% NMP.

The polymer solution temperature was 53°C, and spinning shaft temperature was 48°C.

15

Results

The resulting properties of the hollow fibre membranes according to the examples are presented in the table below.

20

Lp = Hydraulic permeability of water (10^{-4} cm/s/bar).

C = Clearance Urea at QB = 200 ml/min, QD =500 ml/min, UF =0 (ml/min).

S β 2M = Sieving Coefficient for β -2-Microglobulin (MW=11,800) measured in whole blood.

25

S IL6 = Sieving Coefficient for Interleukin6 (MW= 26,000) measured in whole blood.

S alb = Sieving Coefficient for Albumin (MW= 68,000) measured in whole blood.

30

Example No.	LP (10^{-4} cm/s/bar)	C (ml/min)	S β 2M	S IL6	S alb	Pore size (nm)
1	218	181	0.98	0.95	0.011	20-40
2	190	182	0.99	0.98	0.146	>100
2	54	178	0.81	0.36	0.002	10-15

Further, it has also been shown that the membranes according to the invention could be used for diffusive high cut-off renal replacement therapy as an effective
5 strategy to achieve good cytokine clearance while minimizing protein loss. Several treatment modes including continuous venovenous hemodialysis (CVVHD), slow efficient dialysis (SLED) and intermittent hemodialysis (IHD) are conceivable.

10 The above-disclosed approach is an feasible method to clear cytokines much more effectively than conventional renal replacement therapies. The method does not require large amounts of sterile substitution fluids and is associated with a significant lower degree of loss
15 of essential proteins like albumin than high cut-off hemofiltration.

CLAIMS

1. A permselective asymmetric hollow fibre membrane for the separation of toxic mediators from blood, comprised of at least one hydrophobic polymer and at least one hydrophilic polymer, characterized in that said membrane allows passage of molecules having a molecular weight of up to 45 000 Daltons in presence of whole blood, and has a molecular weight exclusion limit in water of about 200,000 Daltons.
2. A membrane according to claim 1, characterized in that said at least one hydrophilic polymer and at least one hydrophobic polymer are present in the membrane as domains on the surface.
3. A membrane according to any of claims 1 or 2, characterized in that said at least one hydrophobic polymer is present in an amount of 50-80 weight%, based on the weight of the membrane.
4. A membrane according to any of claims 1-3, characterized in that said at least one hydrophilic polymer is present in an amount of 20-50 weight%, based on the weight of the membrane.
5. A membrane according to any of claims 1-4, characterized in that said at least one hydrophobic polymer is chosen from the group consisting of polyarylethersulfone (PAES), polypropylene (PP), polysulfone (PSU), polymethylmethacrylate (PMMA), polycarbonate (PC), polyacrylonitrile (PAN), polyamide (PA), or polytetrafluorethylene (PTFE).
6. A membrane according to any of claims 1-5, characterized in that said at least one hydrophilic polymer is chosen from the group consisting of polyvinylpyrrolidone (PVP), polyethyleneglycol (PEG), polyvinylalcohol (PVA), and copolymer of polypropyleneoxide and polyethyleneoxide (PPO-PEO).

7. A membrane according to any of claims 1-6,
c h a r a c t e r i z e d in that said membrane has at
least a 3-layer asymmetric structure.

8. A membrane according to any of claims 1-7,
5 c h a r a c t e r i z e d in that a separation layer is
present in the inner most layer of the hollow fibre.

9. A membrane according to claim 8,
c h a r a c t e r i z e d in that the separation layer
has a thickness of $< 0.5 \mu\text{m}$.

10 10. A membrane according to any of claims 8 or 9,
c h a r a c t e r i z e d in that the separation layer
contains pore channels.

11. A membrane according to any of claims 1-10,
c h a r a c t e r i z e d in that the pore size in the
15 separation layer is 15-60 nm, preferably 20-40 nm.

12. A membrane according to any of claims 1-11,
c h a r a c t e r i z e d in that the sieving
coefficient for IL-6 in presence of whole blood is 0.9-
1.0.

20 13. A membrane according to any of claims 1-12,
c h a r a c t e r i z e d in that the sieving
coefficient for albumin in presence of whole blood is
below 0,05.

14. A membrane according to any of claims 1-13,
25 c h a r a c t e r i z e d in that the openings of the
pores on the outer surface are in the range of $0.5\text{-}3 \mu\text{m}$
and the number of said pores are in the range of 10,000
to 150,000 pores/ mm^2 , preferably 20,000 to 100,000
pores/ mm^2 .

30 15. A membrane according to claim 14,
c h a r a c t e r i z e d in that said membrane has a
four-layer asymmetric structure, and wherein said fourth
outer layer has the form of a sponge layer having the
outer surface according to claim 14.

35 16. Process for the preparation of a membrane
according to claims 1-15 by solvent phase inversion
spinning, comprising the steps of

a) dissolving the at least one hydrophobic polymer and the at least one hydrophilic polymer in a solvent to form a polymer solution,

b) extruding the formed polymer solution through an
5 outer ring slit of a nozzle with two concentric openings,

c) extruding a centre fluid through the inner opening of the nozzle, and

d) subsequently washing and preferably drying the membrane, wherein the polymer solution comprises 10-20
10 weight% hydrophobic polymer and 2-11 weight% hydrophilic polymer.

17. Process according to claim 16, wherein the centre fluid comprises 45-60 weight% of a precipitation medium chosen from the group of water, glycerol and other
15 alcohols.

18. Process according to any of claims 16 or 17, wherein the centre fluid comprises 40-55 weight% of solvent.

19. Process according to any of claims 16-18,
20 wherein the polymer solution emerges from the outer slit opening is, on the outside of the precipitating fibre, exposed to a humid steam/air mixture.

20. Process according to claim 19, wherein the temperature of the humid steam/air mixture is at least
25 15°C, preferably at least 30°C, and not more than 75°C, preferably not more than 60°C.

21. Process according to any of claims 19 or 20, wherein the relative humidity in the humid steam/air mixture is between 60 and 100%.

30 22. Process according to any of claims 19-21, wherein the solvent content in the humid steam/air mixture is between 0,5 and 5 weight% related to water content.

23. Process according to any of claims 16-22,
35 wherein the polymer solution contains 0.5-7.5 % by weight of suitable additives.

24. Process according to any of claims 16-23,
wherein the solvent is chosen from the group comprising,
n-methylpyrrolidon (NMP), dimethylacetamid (DMAC), di-
methylsulphoxide (DMSO), dimethylformamide (DMF),
5 butyrolactone and mixtures of said solvents.

25. Process according to any of claims 16-24,
wherein the temperature at the spinning nozzle and of the
polymer solution and centre fluid, is between 30°C and
80°C.

10 26. Use of a membrane according to any of claims 1-
15 in hemofiltration of whole blood for treatment of
toxic mediator related diseases.

27. Use of a membrane according to any of claims 1-
15 in hemodialysis of whole blood for treatment of toxic
15 mediator related diseases.

28. Use of a membrane according to any of claims 1-
15 in hemodiafiltration of whole blood for treatment of
toxic mediator related diseases.

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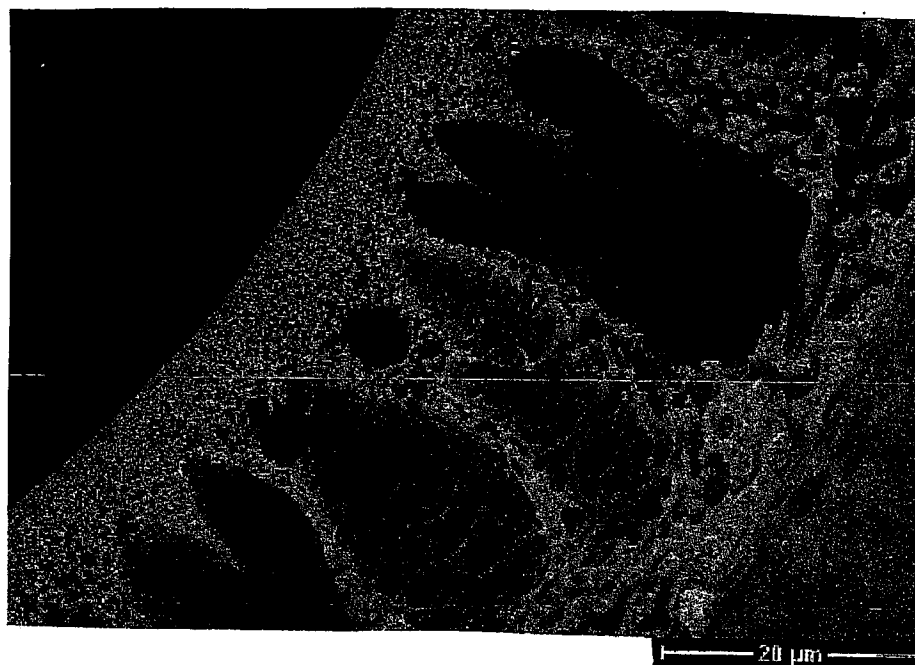


Fig 1a

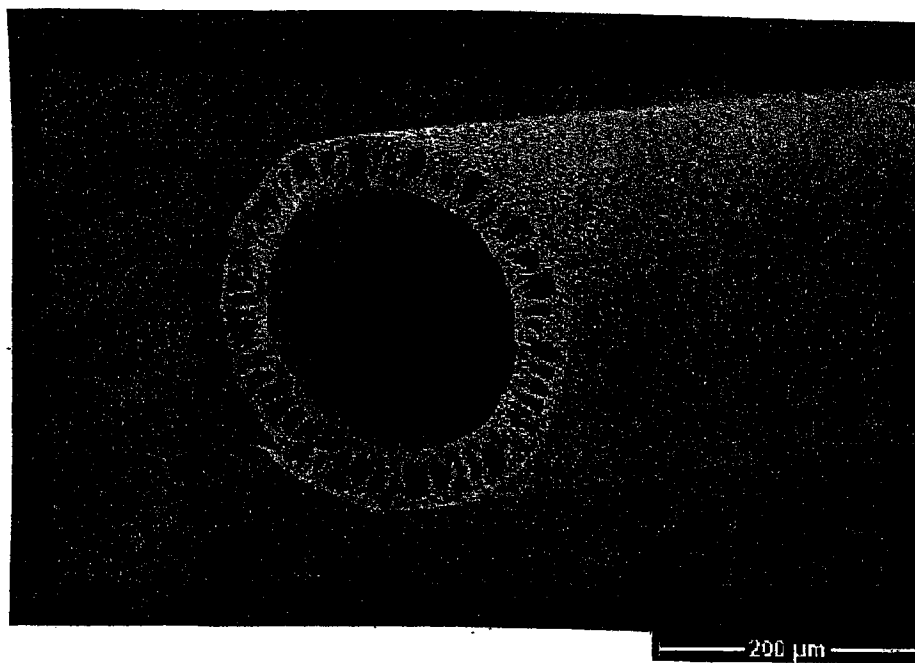


Fig 1b

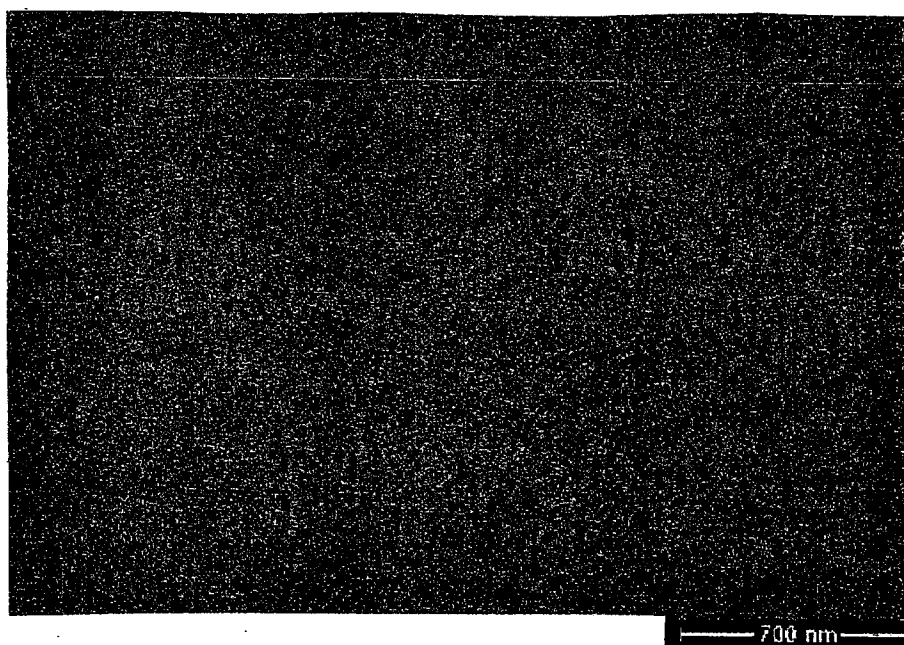


Fig 2

Sieving Coefficients of Polyflux S (High Flux Membrane)
measured in whole blood and buffer (water) - solution

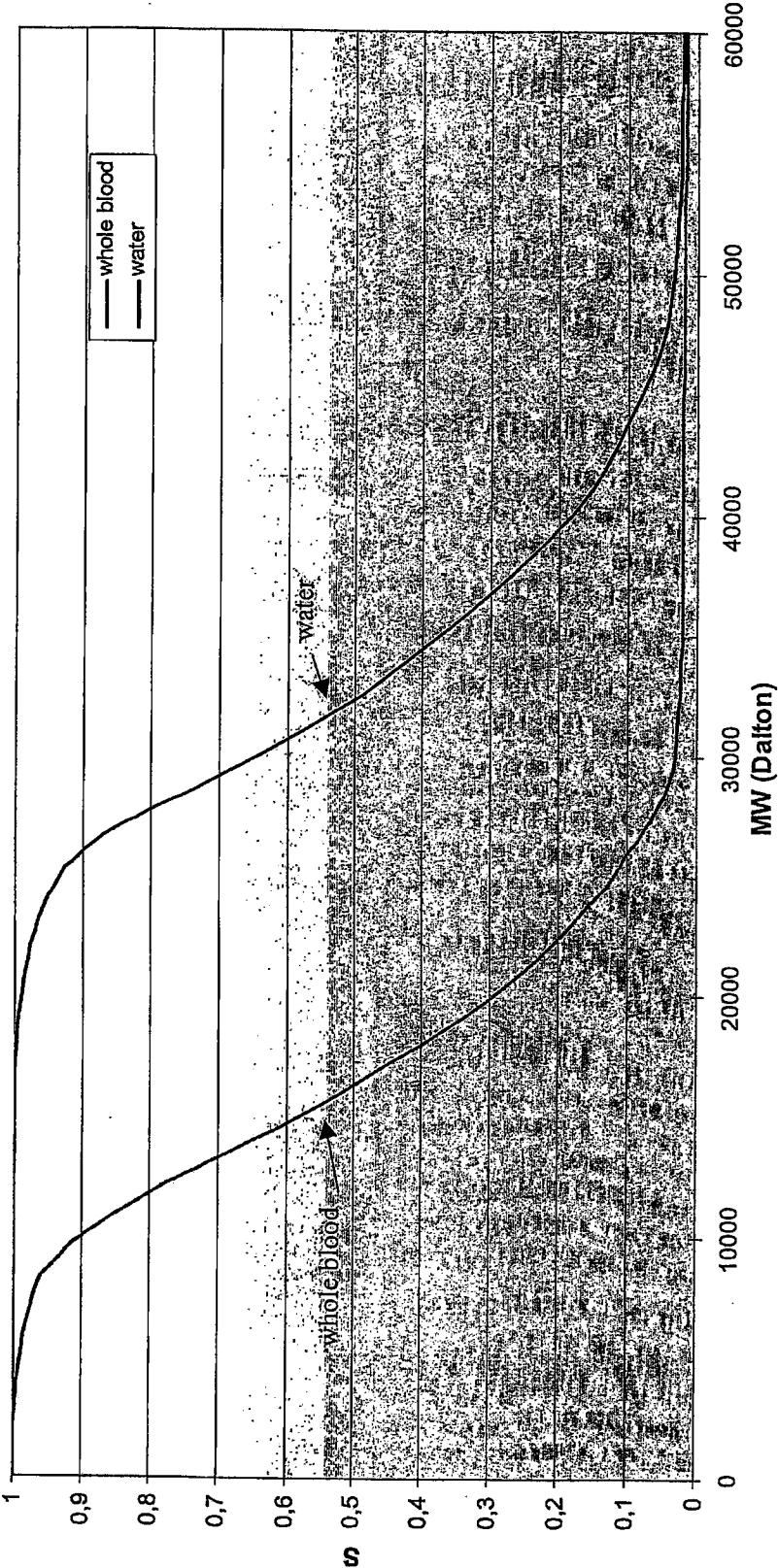


Fig 3a

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Sieving Coefficients of High Cut Off Membrane
measured in whole blood and buffer (water) - solution

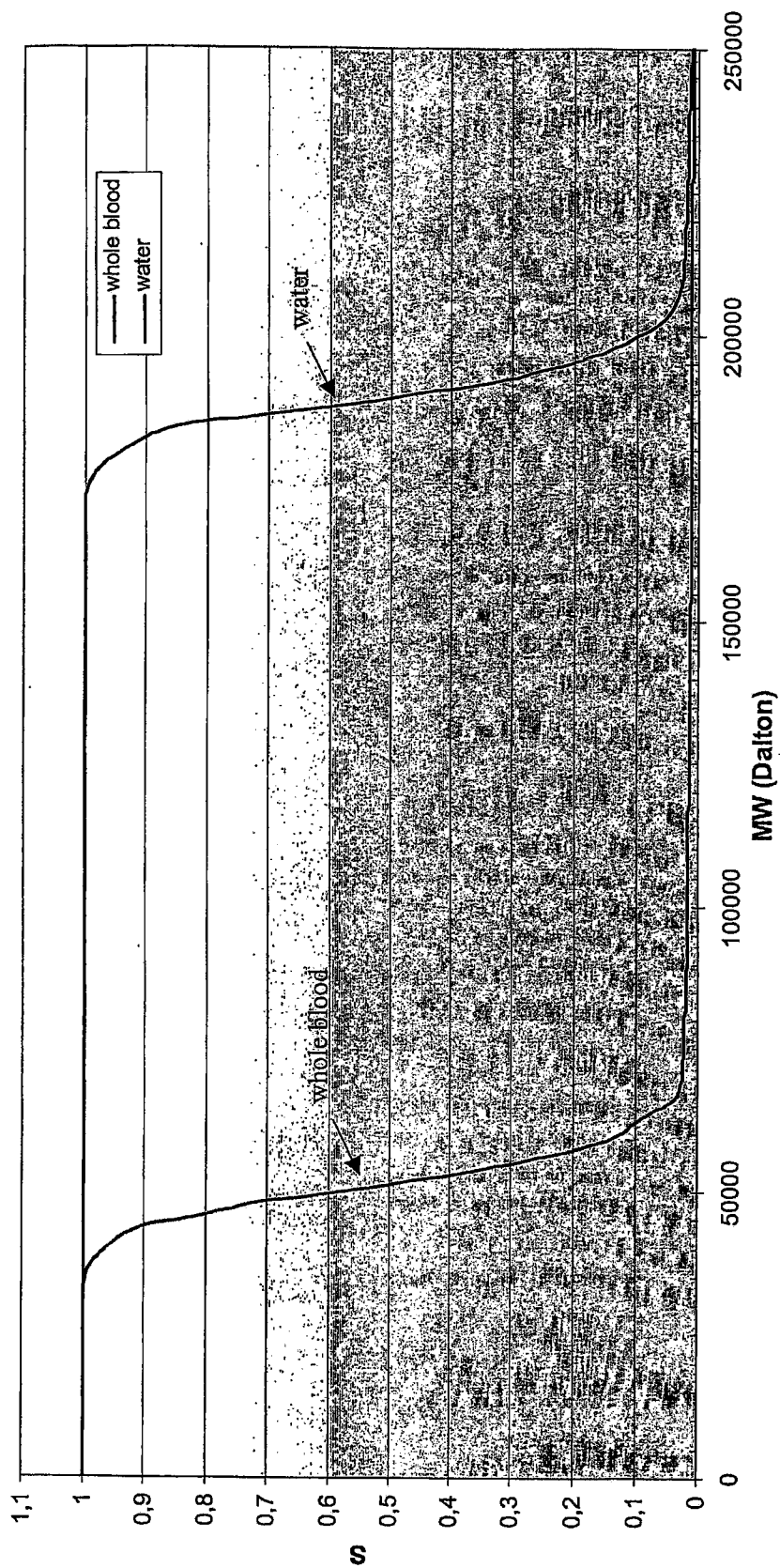


Fig. 3b

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Protein loss into filtrate

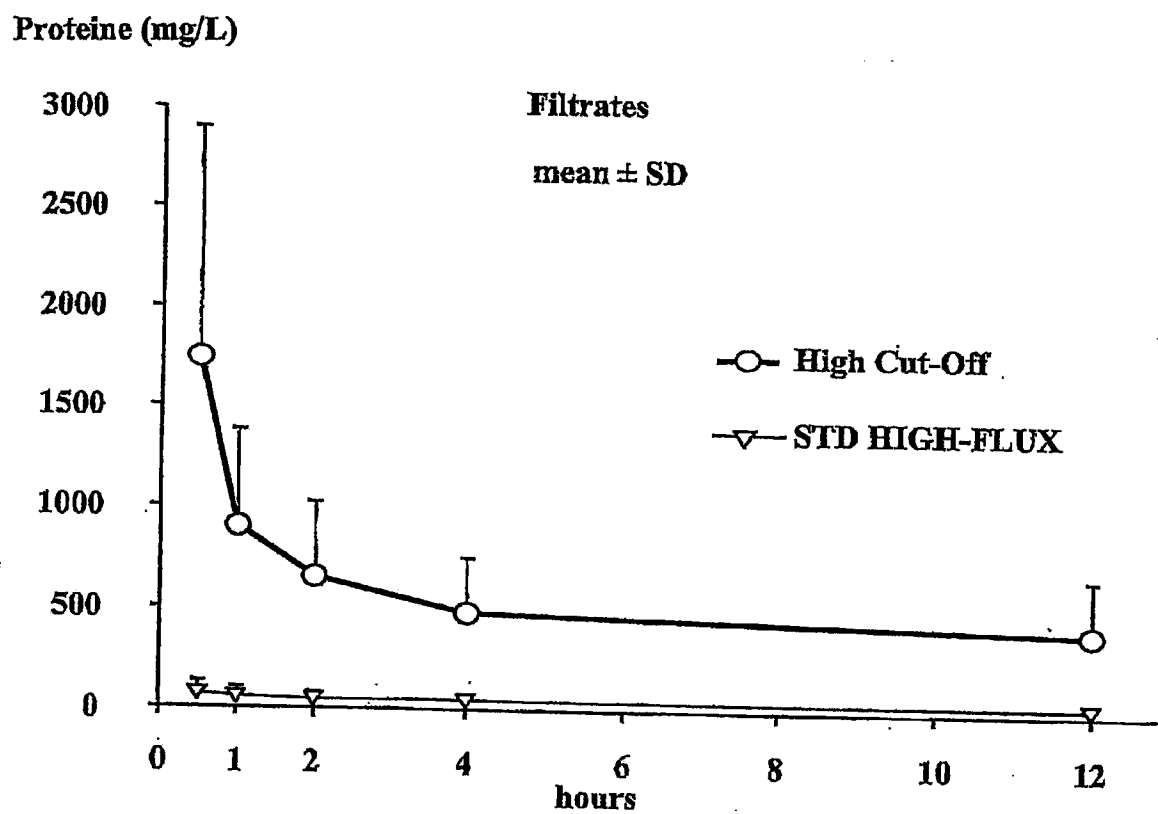
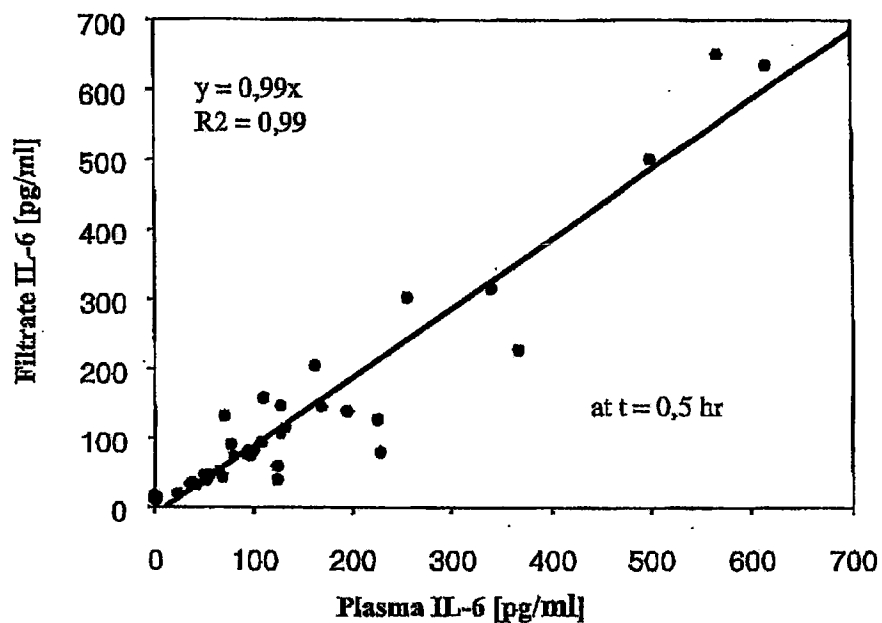


Fig 4

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IL-6 values in plasma and filtrate 30 min after initiation of high cut off filtration.



	Interleukine-6 Sieving Coefficient				
	0,5 hr	1 hr	2 hr	4 hr	12 hr
High Cut-Off	0,92±0,31	0,93±0,32	0,93±0,30	0,88±0,28	0,75±0,33
30kD std HF	0,03±0,05	0,01±0,03	0,01±0,02	0,01±0,02	0,00

Fig 5

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Removal of circulating mediators I RIC/sepsis
-Acute renal failure

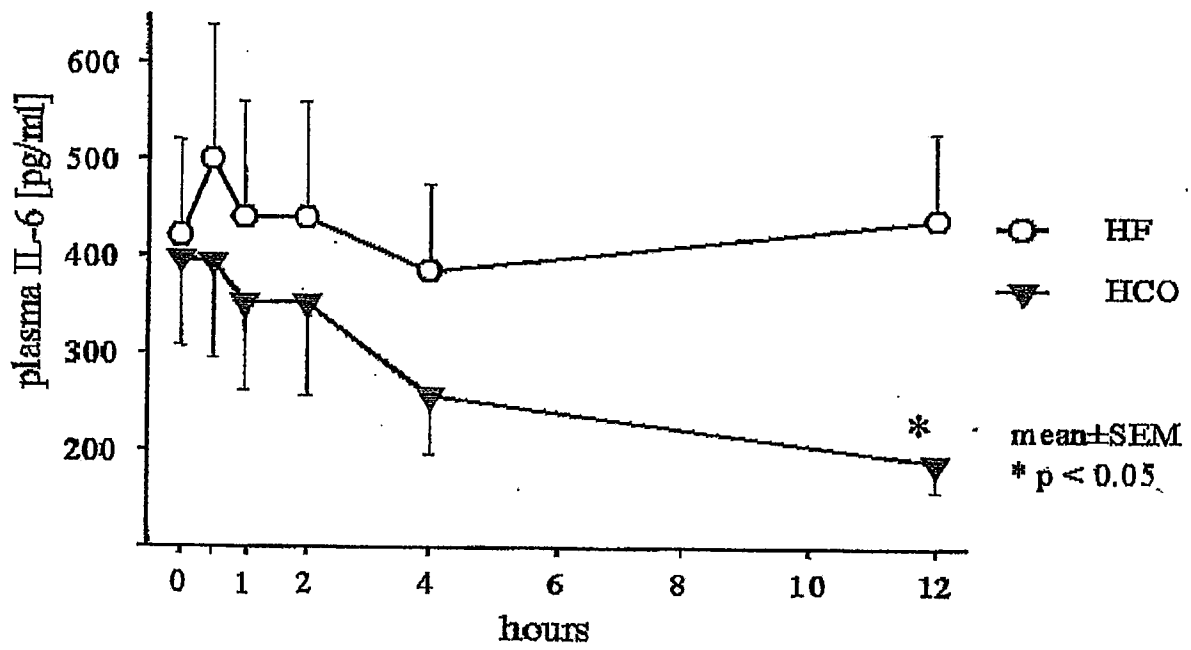


Fig 6

INTERNATIONAL SEARCH REPORT

International application No.

PCT/SE 2003/001993

A. CLASSIFICATION OF SUBJECT MATTER

IPC7: B01D 69/08, D01D 5/24, B01D 71/06

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC7: B01D, D01D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

WPI DATA, EPO-INTERNAL

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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Y	--	3-4,14-15, 17-22
Y	EP 0082433 A2 (HOECHST AKTIENGESSELLSCHAFT), 29 June 1983 (29.06.1983), abstract	3,4
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☒ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

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Date of the actual completion of the international search

8 March 2004

Date of mailing of the international search report

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INTERNATIONAL SEARCH REPORT

International application No.
PCT/SE 2003/001993

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

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27/02/2004

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